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A result analysis of H-slot circular polarized micro strip patch antenna using CST

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Abstract:

The paper describes a novel differential-fed aperture reception apparatus designed for circularly polarized (CP) radiation. This apparatus is characterized by its simplicity in structure and is fabricated on a single layer overlay using standard printed-circuit-board (PCB) technology. Circular polarization is achieved through a dual loop-like strips design with peripatetic wave sharing serving as the transmitting part. The proposed antenna is positioned as a promising candidate for various consumer-level millimeter-wave (mmWave) band applications due to its advantages of wide bandwidth, high gain, simple structure, low cost, and ease of manufacture with differential circuits.

Keywords:

Aperture antenna, circular polarization (CP), Substrate Integrated Waveguide (SIW), 60 GHz.



1. Introduction:

In recent years, there has been a growing demand for high-speed communication in short-range mm-wave wireless personal area networks (WPANs). Circularly polarized (CP) antennas are among the most attractive antenna types due to their characteristics of reduced loss due to misalignment between transmitter and receiver antennas, and excellent mobility in multipath environments caused by surrounding objects and the ground.With the rapid advancement of wireless technologies, ubiquitous and always-on wireless connectivity in homes and enterprises is expected to emerge in the near future. Furthering these existing wireless networks is one of the overarching goals of fourth-generation (4G) wireless technology being discussed globally today. A comprehensive framework of heterogeneous networks, including wireless personal area networks (WPANs), wireless local area networks (WLANs), cellular, Wi-MAX, and satellite systems, can be integrated into 4G technologies. In this article, we discuss advancements and challenges for deploying next-generation short-range wireless systems focusing on three technologies: Ultra-Wideband (UWB), sixty GHz millimeter-wave-based WPAN, and ZigBee. We provide a summary of key technical choices, standardization, regulations, as well as highlight issues for successful deployment. The wireless Medium Access Control (MAC) protocol of sixty GHz WPAN is also addressed.

The mobile terminal (MT) will Communicate with various terminals through millimeter-waves. The information rate which may be transmitted by the terminal is almost 1-Gbps. A regenerative-repeater-type access point terminal (APT) is likewise created to grow correspondence differ between MTs. In this work, another differentially-fed CP opening recieving wire is proposed. The reception apparatus utilizes just a solitary layer of substrate with substrate integrated waveguide (SIW) for its nourishing. A couple of circle like strips with voyaging wave excitation on the upper expansive mass of the SIW is utilized to produce CP radiation inside a rectangular opening while a cavity made of the SIW's metalized vias and base ground is utilized to offer good unidirectional radiation and higher pick up.

The rising 60 GHz system has adequately expansive recurrence band that is equipped for taking care of the vital high information rate (up to various Giga bits every second). Related with this kind of utilizations is the requirement for a mandate, wideband, low misfortune, and ease radio wire that can be effectively incorporated with the mm-wave hardware of a handset bundle [4, 5].

As a general rule, there is little investigation on elite minimal effort CP opening recieving wires in like manner and on mm Wave CP planar gap reception apparatuses in careful. A portion of this examination contain a curved gap horn radio wire with septum roundabout polarizer work at 4.7 GHz and create by methods for metal cutting, which will be assessed in [12]. The reception apparatus finishes an impedance transmission capacity for articulation coefficient $S11\leq-10$ dB of22%, a 3-dB AR data transfer capacity of 18% and a most extreme pick up of 12.5 dBi. An artificial magnetic conductor (AMC) reflector back opening radio wire oversee at 6 GHz and manufacture utilizing multilayer PCB system was anticipated in [13], which achieve an impedance data transfer capacity of around 36%, a 3-dB AR transmission capacity of 33%, and a relentless pick up roughly 7 dBi over the apply band. An unpredictable pit supported radio wire at 2.6 GHz that is invigorated by cross triangular tie dipoles notwithstanding feed by a microstrip line to double opening line adjustment was present in[14], which accomplish an impedance data transmission of 57%, an AR transfer speed of 39% and a pinnacle pick up of 10.7 dBi. In [15], a gap cluster recieving wire of 16×16-components with a corporate-feed empty waveguide circuit was anticipated at 60 GHz, which accomplish an impedance data transfer capacity of 5.7%, an AR transmission capacity of 6.4% and pinnacle pick up of 33.3 dBi

2. System design:

2.1. Basic configuration:

At the specially appointed gathering, numerous remote terminals will speak with each other over a fleeting system. Fast data transmission interfaces between terminals additionally are outlined inside a little territory. For millimeter-wave transmissions, the transmission separate is confined because of the low radiation control (10 mW for unapproved usage) and high engendering way misfortune. Multipoint-to multipoint associations are workable for little space, nonetheless, expanding the correspondence region is possible when a few systems are associated utilizing multi-jump association.

The design of the anticipated reception apparatus is appeared in Fig.1. The reception apparatus comprises of a double circle like strips arrangement, are rectangular gap, and a best opening depression. Here, the strips development could be depicted as two indistinguishable arrangements of strips, where each set is made out of a couple of rotationally symmetrical twisted strips. The double circle arrangement is carved at the focal point of the gap on the upper metal mass of the substrate integrated waveguide (SIW) with the outward strips associated with



be external encouraged at the gap edge. The depression is found straightforwardly underneath the gap.

2.2. Geometry of proposed antenna:

The geometry of H-Slot Dual Band Micro strip Patch radio wire comprise a coaxial feed rectangular fix printed over FR4 substrate of thickness h=1.5 mm, dielectric consistent ϵ r=4.3, and digression misfortune is 0.019 as appeared in Fig.1. H-space is cut on the fix's surface isolated by GND plane Lg ×Wg= 26 × 32 mm. The GND plane and fix is isolated by substrate. The measure of H-Slot Dual Band Micro strip Patch reception apparatus is ascertained by utilizing Standard equations for microstrip fix radio wire outline. Table 1 speaks to the measurements of proposed radio wire which is intended to accomplish Multi band.

The electromagnetic vitality going inside the SIW is coupled into the opening region through the external strips from the two inverse feed focuses. Contrasted with the customary qui rakish winding reception apparatuses sustained at the inside with broadband adjusted structures [14], the displayed recieving wire is basically external fed at the opening edge by decreased augmentations of the upper mass of the SIW. This encouraging technique dispenses with the requirement for the multi-layer setup that is natural on account of winding radio wire plan. This makes the proposed recieving wire simple to coordinate with mm-wave circuits in the minimal effort planar PCB innovation.

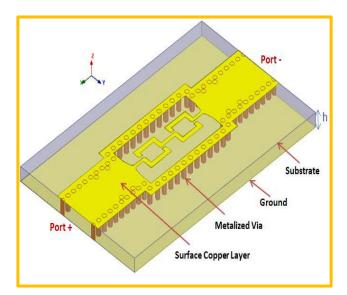


Figure. 1: (a) Perspective view

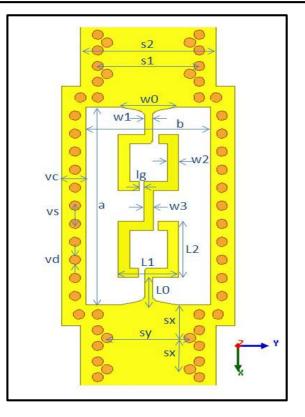


Figure. 1: (b) Top view

Fig. 1 Geometrical configuration of the proposed antenna.

Table. 1: Design parameters of the proposed antenna

Parameter	LO	L1	L2	w0	w1	w2	W3	lg	h
Value (mm)	0.88	1.6	1.8	1.5	0.2	0.3	0.25	0.15	0.79
Parameter	vd	vs	vc	a	b	sx	sy	S 1	S2
Value (mm)	0.3	0.55	0.65	6.3	3.3	1.2	2.2	2.8	3.6

Para- meter	LO	L1	L2	wO	w1	w2	w3	lg	h
Value (mm)	0.88	1.6	1.8	1.5	0.2	0.3	0.25	0.15	0.79
Para- meter	vd	vs	vc	a	Ь	sx	sy	s1	<u>\$2</u>
Value (mm)	0.3	0.55	0.65	6.3	3.3	1.2	2.2	2.8	3.6

3. Antenna measurement:

Geometrical parameters of the proposed recieving wire were upgraded through recreations by methods for the electromagnetic (EM) programming CST. A rundown of the utilized plan



parameters esteems is given in Table I. mimicked Measurements comes about for reflection coefficient (S11), axial ratio (AR), pick up are accomplished. Due to the system's constraint, just recurrence information up to 67GHz and outflow model in the upper side of the equator were estimated.

3.1. Differential feeding network:

Practically speaking, there is no requirement for differential nourishing system when coordinating the proposed reception apparatus with differential mm Wave circuits. Nonetheless, since the accessible estimation system is single-finished, an inflatable is important to do the estimations. The differential feeding system depends on E-plane tee [15]. The contribution of the differential sustaining system is a WR-15 waveguide, which is secured to the expansive mass of a SIW. The coupling of vitality from the WR-15 waveguide to the two arms of the SIW is accomplished by methods for E-field as the waveguide's hub and the E-field vector plane of the SIW are parallel. The vitality streaming out into one arm is normally out of stage to the next arm. Along these lines, a great differential flag can be gained from the two arms of the SIW. Fig. 2 gives a conceivable topology for incorporating the proposed reception apparatus with a differential mm Wave coordinated circuit (IC) as radio wire in-bundle. The bundle comprises of two substrates (Sub1 and Sub2) with three metal layers (M1, M2 and M3). The IC is bound on metal layer M1 on the base of Sub1. The reception apparatus is actualized on Sub2 between metal layers M2 and M3, where M2 additionally shapes the recieving wire's ground. The reception apparatus is feeded differentially by two metalized vias on its two closures, which interface with the RF differential info/yield of the IC.

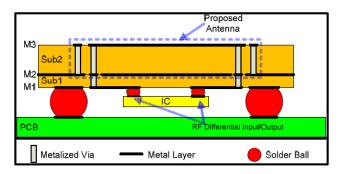


Figure. 2: Possible topology of integrating the proposed differential antenna with a differential mm Wave IC in the form of antenna-in-package

4. Simulation results and discussion:

Geometrical requirement of the proposed recieving wire was upgraded through recreations utilizing the business electromagnetic (EM) programming and CST. A rundown of the utilized outline parameters esteems is given in Table. I. To check the proposed plan, a reception apparatus model was manufactured and tried. Estimations for reflection coefficient (S11) were gotten utilizing Agilent E8361A arrange analyzer and estimations for axial ratio (AR), pick up and radiation design were acquired utilizing NSI Near field System. Because of the system's restriction, just recurrence information up to 67GHz and radiation design in the upper half of the globe were estimated. The reception apparatus and radiation productivity 92% accomplished after reenactment of proposed the radio wire is executed onSub2 between metal layers M2 and M3, where M2 additionally shapes the recieving wire's ground. The reception apparatus is fed differentially by two metalized vias on its two closures, which interface with the RF differential info/yield of the IC. Simulated and estimated aftereffects of S11 of the proposed reception apparatus are appeared in Fig. 3(a) and great assention is watched.

The simulated - 10-dB impedance data transfer capacity is 21% (56-69 GHz) contrasted with more than 24% (54-69 GHz) for estimation. Mimicked and estimated aftereffects of AR are delineated in Fig. 3(b), which demonstrates a recreated 3-dB AR data transfer capacity of 17.9% (55.5-66.5 GHz) contrasted with 16.3 % (56.5-66.5 GHz) for estimation. Fig. 3(c) demonstrates a mimicked 3-dB RHCP pick up transfer speed of 21% (54.5-67.5GHz) contrasted with a deliberate pick up data transfer capacity of 18.7% (55.5-67 GHz). In the interim, crest pick up is 11.8 and 12.4 dBi, both at 66 GHz, for reenactment and estimation, individually.

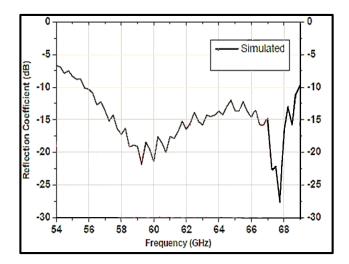


Figure. 3 :(a) Reflection Coefficient



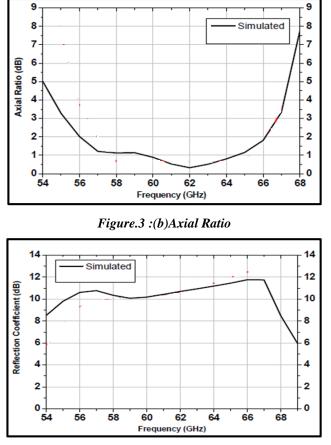


Figure.3: (c) Broadside RHCP Gain

Fig. 3. Simulated and measured performance results of proposed antenna.

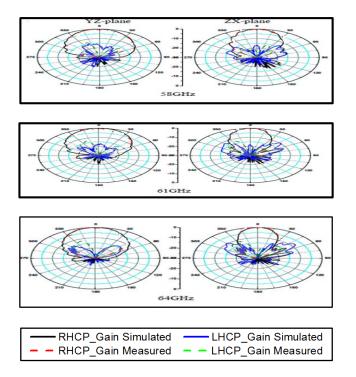


Fig. 4. Replicated and calculated energy patterns of the proposed antenna at different frequencies within the operating bandwidth.

Fig. 4 demonstrates simulated and estimated consequences of the standardized radiation examples of the radio wire at various frequencies inside the working data transfer capacity. As can be seen, the radiation designs at both YZ-and ZX-planes are exceptionally symmetric and both mimicked and estimated comes about match extremely well. The recieving wire is unmistakably RHCP with its primary bar and henceforth, the greatest increase settled in the broadside bearing. The simulated and estimated standardized radiation designs show cross-polarization levels of not exactly - 12 dB on the two planes. In the meantime, the front-to-back proportion is bigger than 20 dB

5. Conclusion:

In this paper a brand new differentially-fed circularly polarised opening radio wire with simple structure and great execution has been illustrated. The outcome in this paper, a brand new differentially-fed circularly polarized aperture antenna with simple structure and great execution has been illustrated. The anticipated plan can be acknowledged on a solitary layer cover utilizing standard printed-circuit-board (PCB) innovation where SIW structure is utilized to make both the encouraging and in this way the top-opening cavity. The anticipated radio wire has the benefits of wideband, high radiation proficiency, planar write, ease, and great mix capacity that fabricate it appropriate for the 60 GHz and other mm-wave applications.

6. References:

- Diaaaldin, J. Bisharat, Shaowei Liao, and QuanXue. "Single-layer differentially-fed circularly polarized aperture antenna for 60 GHz applications" 9th European Conf. on Antennas and Propag. (EuCAP). IEEE, 2015.
- (2) Takeshi Fukusako and Teruhisa Nakamura, "Broadband Design of Circularly Polarized Microstrip Patch Antenna Using Artificial Ground Structure With Rectangular Unit Cells" IEEE Trans. on Antennas and Propag.volu. 59, NO.6, June 2011.
- H. Ogawa, "Millimeter-wave wireless personal area network systems" Proc. Radio Freq. Integrated Circu.Symp., San Francisco, CA,USA, Jun. 2006, 11–13.
- (4) H.K. Lau, "High-speed short-range systems for wireless personal area networks" Wireless Tele. Comm. Symp. Apr. 2009, pp. 1-4.

- (5) S. Emami et al., "A 60GHz CMOS phased-array transceiver pair for multi-Gb/s wireless communications" Proc. IEEE Intl. Solid-State Circuits Conference Dig.ofTechn. Papers (ISSCC), pp.164-166, Feb. 2011.
- (6) L. Li et al., "Design of 60GHz RF transceiver in CMOS: Challenges and recent advances" Communications, China, vol. 11, no. 6, pp.32-41, Jun. 2014.
- (7) C. R. Liu, Y. X. Guo, X. Y. Bao, and S. Q. Xiao, "60-GHz LTCC Integrated Circularly Polarized Helical Antenna Array" IEEE Trans. Antennas Propag., vol. 60, no. 3, pp. 1329-1335, Mar. 2012.
- (8) KaushikMandal and ParthaPrtimSarkar "High Gain Wide-Band U-Shaped Patch Antennas with Modified Ground Planes" IEEE Trans. on Antennas and Propag., vol. 61, no.4,pp.2279-2282,April 2013.
- (9) Ahmed Khidre, Kai-Fong Lee, Fan Yang, and Atef Z. Elsherbeni, "Wide Band Dual Beam U-Slot Microstrip Antenna" IEEETrans. On Antennas and Propag., vol. 61, no. 3, pp.1415-1418, March 2013.
- (10) Juhua Liu and QuanXue, "Broadband Long Rectangular Patch Antenna with High Gain and Vertical Polarization" IEEE Trans. on Antennas and Propag., volume 61, no.2, February 2013.
- (11) Kwai-Man and LukMingjian Li "A Low-Profile Wideband Planar Antenna" IEEE Transactions on Antennas and Propagation, VOL. 61, NO. 9, pp.4411-4418, September 2013.
- (12) Ahmed Khidre, Kai-Fong Lee, Fan Yang, and Atef Z. Elsherbeni "Circular Polarization Reconfigurable Wideband E-Shaped Patch Antenna for Wireless Applications" IEEE Trans. on Antennas and Propag., vol. 61, no.2, pp.960-965, February 2013.
- (13) Jianyi Zhou and WenwenYang, "Wideband Low-Profile Substrate Integrated Waveguide Cavity-Backed E-Shaped Patch Antenna" IEEE Trans. on Antennas and Propag., vol.12, 2013.
- (14) S. Bhunia, "Effects of Slot Loading on MicrostripPatch Antennas" International Journal of Wired and Wireless Communications, volume 1, issue 1, October, 2012.
- (15) Kanchan Cecil and PurvaiRastogi, "S and C Bands Multilayer T-Slot Photonic Band gap Micro Strip Antenna" IOSR Journal of Engineering, vol. 2(4), April 2012.

- (16) S. T. Fan, Y. Z. Yin, B. Lee, "Bandwidth Enhancement of a Printed Slot Antenna with a Pair of Parasitic Patches" IEEE Transactions on Antenna and Wireless Propag. vol. 11, 2012.
- (17) D. M.Pozar, "Microwave Engineering. New York: Addison-Wesley" 1990, p. 185.
- (18) C. A. Balanis, "Antenna Theory: Analysis and Design. New York: Wiley" 1997, p. 734.
- (19) X.F. Liu et al, "Design of a low profile modified U-Slot Microstrip Antenna Using PSO Based on IE3D" Microwave and optical Techn. Letters, Volume 49, No.5, .1111-1114, May, 2007.
- (20) S. I. Latif, L. Shafai, and S. K. Sharma, "Bandwidth Enhancement and Size Reduction of Microstrip Slot Antenna" IEEE Trans. on AntennasProp. vol. 53, 994–1003, March, 2005.
- (21) Shao Wei Liao, QuanXue, Fellow, IEEE, and JianHuaXu"Parallel Plate Transmission Line and L-Plate FeedingDifferentially Driven H-Slot Patch Antenna"IEEE Antennas and Wireless Propagation, vol. 11, 640-644, 2012.